

[0021] In an embodiment, the summing amplifier is configured to transmit the trip signal to a relay configured to cut off the current in response to the trip signal.

[0022] According to some exemplary embodiments of the invention, there is provided a system including: a load; a power source configured to supply power to the load; a switch coupled between the power source and the load; and a protection circuit configured to sense a load current passing through the load and to generate a trip signal indicative of an overcurrent condition, the protection circuit including: a first current integrator and a second current integrator, each of the first and second integrators being configured to integrate an input voltage proportional to the load current; a summing amplifier configured to receive an offset voltage, to amplify a signal from the second integrator, and to generate a dynamic trip threshold based on the input voltage and the offset voltage; and a comparator configured to compare an output of the first current integrator and the dynamic trip threshold, and to generate a trip signal at a trip time when the dynamic trip threshold is equal to an output of the first integrator, the trip signal indicating an overcurrent condition, and wherein the switch is configured to actuate in response to receiving the trip signal, and to stop current flow from the power source to the load.

BRIEF DESCRIPTION OF THE DRAWINGS

[0023] The above and other features and aspects of the invention will become more apparent by the following detailed description of exemplary embodiments thereof with reference to the attached drawings, in which:

[0024] FIG. 1 is a diagram illustrating an ideal I^2t trip characteristic of an electronic protection device;

[0025] FIG. 2 is a block diagram illustrating a system utilizing a protection circuit according to some exemplary embodiments of the invention;

[0026] FIG. 3 is a block diagram illustrating a protection circuit according to some exemplary embodiments of the invention;

[0027] FIG. 4 is a circuit diagram illustrating the protection circuit of FIG. 3 according to some exemplary embodiments of the invention; and

[0028] FIG. 5 is a diagram comparing the ideal I^2t trip characteristic with that of the approximated I^2t trip characteristic of the protection circuit according to some exemplary embodiments of the invention.

DETAILED DESCRIPTION

[0029] The attached drawings for illustrating exemplary embodiments of the invention are referred to in order to gain a sufficient understanding of the invention, the merits thereof, and the objectives accomplished by the implementation of the invention. The invention may, however, be embodied in many different forms and should not be construed as being limited to the exemplary embodiments set forth herein; rather, these exemplary embodiments are provided so that this disclosure will be thorough and complete, and will fully convey the concept of the invention to those skilled in the art.

[0030] Hereinafter, the invention will be described in detail by explaining exemplary embodiments of the invention with reference to the attached drawings. In the drawings, like reference numerals are used throughout the figures to reference like features and components.

[0031] FIG. 2 is a block diagram illustrating a system 100 utilizing a protection circuit 110 according to some exemplary embodiments of the invention.

[0032] Referring to FIG. 2, the system 100 may include a power source 102, a load 104 powered by the power source 102 through a conductor (e.g., a wire) 106, a switch (e.g., relay) 108 for switchably connecting the power source 102 and the load 104 (i.e., the switch 108 is located in a current path between the power source 102 and the load 104), and a protection circuit 110 for monitoring the current I passing through the conductor 106 and controlling the operation (e.g., activation and deactivation) of the switch 108 based on the monitored current I .

[0033] According to some embodiments, the protection circuit 110 maintains the switch 108 in an activated state (e.g., a closed or turned ON state) when the conductor current I is at a level that does not exceed the thermal capacity of the conductor 106, and deactivates (e.g., opens, turns OFF, or “trips”) the switch 108 when the thermal capacity of the conductor 106 is reached or exceeded. The trip characteristic of the protection circuit 110 may be substantially similar to that shown in FIG. 1, where the protection circuit 110 ensures that the current-supplying operation of the system 100 is confined to region A (e.g., the area below the curve 10) in FIG. 1 and does not reach region B (e.g., the area above the curve 10) in FIG. 1. For example, the protection circuit 110 deactivates the switch 108 within about 100 millisecond of a current, which is 10 times higher than the conductor's rated current, passing through the conductor 106. In some examples, deactivation may occur within about 4 seconds of passage of a current that is twice the rated current.

[0034] Thus, the protection circuit 110 isolates a fault in the system 100 (e.g., a short circuit in the load 104) in a timely manner, by preventing an overcurrent condition that exceeds the thermal capacity of the conductor 106.

[0035] The protection circuit 110 may sense (e.g., measure) the current I using a sense resistor, a hall effect sensor, and/or any other suitable means known to a person of ordinary skill in the art. The switch 108 may be an electro-mechanical relay, a solid state switch, or the like.

[0036] FIG. 3 is a block diagram illustrating a protection circuit 110 according to some exemplary embodiments of the invention.

[0037] In some embodiments, the protection circuit 110 may include a first current integrator 112, a second current integrator 114, a summing amplifier 116 and a comparator 118. Each of the first and second current integrators 112 and 114 integrates an input voltage V_{Curr} that is proportional to the sensed current I . In some examples, the input voltage V_{Curr} represents a voltage output of a current sensor within the protection circuit 110 measuring the sensed current I . The summing amplifier 116 amplifies a signal from the second current integrator 114 to generate a trip threshold (e.g., a dynamic trip threshold) that is based on the input voltage V_{Curr} (which is proportional to the current I). The comparator 118 compares the output of the first current integrator 112 with the trip threshold, and generates a trip signal S_{Trip} when the comparative relationship between the output of the first current integrator 112 and the trip threshold has changed. For example, upon being tripped, the comparator 118 may output a voltage that is higher (or lower) than that outputted before being tripped.